#### **Abstract**

Nowadays, several applications ask for some kind of synchronization between the different motors. Example because of the large output power required for the long production line, conveyor line or assembly line in the industrial producing process, a single motor can't achieve the required output torque. So in this situation, two or more motors are necessarily applied to complete the control tasks synchronously and coordinately.

The principle, on which this control scheme is based, is called the master slave motors control. The master motor is the reference motor to which one or more slave motors are synchronized. Its main characteristic is that the revolving speed output of the master motor will be the reference value of the slave motor. Any input signal or disturbance on the master motor can be reflected and followed by the slave motor.

The main objective of this research is to develop a mean of synchronizing two induction motors based on master-slave strategy, by designing a speed control system for the two induction motors. Mathematical model for the induction motor has been derived and tested using simulink in open-loop direct start-up mode, also a simulink model for PWM inverter. Vector control technique use PI controller has been used for both the master and slave motors. The simulation results obtained using simulink showed a better tracking performance with acceptable tracking error.

#### المستخلص

في الوقت الحاضر، هنالك عِدّة تطبيقات تعتاج لفوع من التزامن بين المحرّكات المختلفة على سبيل المثال بسبب قهرة الخرج الكبيرة المطلوبة لخَطِّ الإنتاج الطويلِ أو الخطِّ الفاقلِ أو خط التجميع في العملية الإنتاجية الصناعية، نجد إن محرّك و احد لا عيمتطيع توفير عزم الخرج المطلوب. لذا في هذة الحالة، محركان أو أكثر تكون ضرورية لتكملة وانجاز عملية التحكم بشكل متزامناً ومتناسقاً.

هذا المبدأ، الذي يستند عليه مخططِ القحكم، يسمّى بتحكم السيد التابع للمحركات. إنّ المحرك السيد هو المحرك الاساسي بينما يكون هنالك محرك تابع أو أكثرِ من مطلوب مُز امَنتها. الخاصيه الرئيسية هي أنّ السرعةِ ال ناتجة من المحركِ السيدِ تكُونُ هي الإشارة الهرجعية للمحركِ التابع. أيّ إشارة دخل أو إضطراب على المحركِ السيدِ يُمْكِنُ عُكَسَها وتتبعها بواسطة الهحركِ التابع.

إنّ الهدف الرئيسي للبحث هو تطوير وسيلة لمزامنة محركين حثيين اعتمادا على استراتيجية السيد القابع، من خلال تصميم نظام تحكم في سرعة محرك ين حثين النموذج الرياضي للمحرك الحثيّ تم إشتقاقه وإختبلوه بلستعمال simulink في الحلقة المفتوحة، أيضا نموذج عاكس تعديل عرض النبضة تم تمثيله بإستخدام simulink. استعملت تقنية التحكم بالمتجهات بإستعمال متحكم تناسبي- تكاملي لكل من محرّكي السيد والقابع نتائج المحاكاة التي تم الحصول عليها بلستعمال simulink واظهرت أداء تتبع جيد بخطأ مقبول.

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## **List of Symbols**

d <sup>e</sup> -q <sup>e</sup>	Synchronously rotating reference frame direct and quadrature
	axes
d <sup>s</sup> -q <sup>s</sup>	Stationary reference frame direct and quadrature axes
f	Frequency (Hz)
$I_{m}$	RMS magnetizing current
$I_r$	RMS rotor current
$I_s$	RMS stator current
i <sub>dr</sub> s	d <sup>s</sup> – axes rotor current
i <sub>ds</sub> s	d <sup>s</sup> – axes stator current
$i_{ m qr}$	q <sup>e</sup> – axes rotor current
$i_{ m qs}$	q <sup>e</sup> – axes stator current
J	Moment of inertia (kg.m <sup>2</sup> )
$X_{ds}$	d <sup>e</sup> – axes synchronous reactance
$X_{ m lr}$	Rotor leakage reactance
$X_{ls}$	Stator leakage reactance
$X_{qs}$	q <sup>e</sup> – axes synchronous reactance
$\theta_{\mathrm{e}}$	Angle of synchronously rotating frame
$\theta_{\rm r}$	Rotor angle
$\theta_{ m sl}$	Slip angle
L <sub>m</sub>	Magnetizing inductance
$L_{\rm r}$	Rotor inductance
$L_{\rm s}$	Stator inductance
$L_{lr}$	Rotor leakage inductance
$L_{ls}$	Stator leakage inductance
$L_{dm}$	d <sup>e</sup> – axes magnetizing inductance
$L_{qm}$	q <sup>e</sup> – axes magnetizing inductance
N <sub>r</sub>	Rotor speed (RPM)
N <sub>s</sub>	Synchronous speed
P	Number of poles
$P_g$	Air-gap power (watt)
$P_{m}$	Mechanical power
$R_{r}$	Rotor resistance (Ohm)
$R_{\rm s}$	Stator resistance
S	Slip (per-unit)
T <sub>e</sub>	Devolved torque (N.m)
$T_{\rm L}$	Load torque
$V_d$	DC voltage (volt)
$V_{g}$	RMS air-gap voltage
V <sub>m</sub>	Peak phase voltage
V <sub>dr</sub> <sup>s</sup>	d <sup>s</sup> – axes rotor voltage
V <sub>ds</sub> <sup>s</sup>	d <sup>s</sup> – axes stator voltage

V	q <sup>e</sup> – axes rotor voltage
V <sub>qr</sub>	
$V_{qs}$	q <sup>e</sup> – axes stator voltage
ф	Displacement power factor angle
Ψa	Armature reaction flux linkage (weber.turn)
$\psi_{\mathrm{m}}$	Peak air gap flux linkage
$\psi_{\rm r}$	Rotor flux linkage
Ψs	Stator flux linkage
Ψ <sub>dr</sub> <sup>s</sup>	d <sup>s</sup> – axes rotor flux linkage
$\psi_{ds}^{\ \ s}$	d <sup>s</sup> – axes stator flux linkage
$\psi_{qr}$	q <sup>e</sup> – axes rotor flux linkage
$\psi_{qr}$	q <sup>e</sup> – axes stator flux linkage
ω <sub>e</sub>	Stator or line frequency (r/s)
$\omega_{\mathrm{m}}$	Rotor mechanical speed
$\omega_{\rm r}$	Rotor electrical speed
$\omega_{\mathrm{sl}}$	Slip frequency
Â	Peak value of sinusoidal phasor or sinusoidal space vector (X any arbitrary variable)