SUDAN UNIVERSITY OF SCIENCE AND TECHNOLOGY FACULTY OF GRADUATE STUDIES

CYLINDER'S LINER WEAR CHARACTERISTICS IN TWIN CRANKSHAFT INTERNAL COMBUSTION ENGINES

خواص التآكل في مبطنات أسطوانات محركات الاحتراق الداخلي ثنائية عمود المرفق

By

Maisara Mohy Eldin Gasim Mohamed

A thesis submitted for the degree of doctor of philosophy in Mechanical Engineering

Supervisor: Prof. Uzaldin S. Abdulhussain

Co-supervisor: Dr. Taj Elssir Hassan

Department of Mechanical Engineering

College of Engineering

2007

Abstract

Conventional internal combustion engines have been around for more than a century. Due to its high efficiency and low cost.

The overall efficiency of IC engines approaches 50%. This means that only about 50% of the fuel is converted into useful work, and the rest of fuel power is useless energy mainly due to friction between moving parts.

Friction is the worst enemy of machinery. It wears out metal, wastes power and generates heat. Friction occurs in all moving parts in the engine, like piston rings, journal bearings, valves and cams. Friction between piston rings, cylinders liner responsible for about half of the usefulness energy ⁽¹⁾.

Sliding contacts between a piston ring and a cylinder liner leads to a variety of different friction mechanisms during one working cycle of the engine. Owing to the variations in load, speed and counter surface effects, lubrication conditions in a ring/liner contact are strongly transient, which is reflected by variations in the friction and wear behavior.

Wear in cylinder liner causes inefficiency seal, and it may result in increased oil consumption, leakage, blow-by, and increasing fuel consumption.

Combustion pressure cause a force on piston, the horizontal component is a side thrust force which is normal to liner wall. This force is responsible for the friction between piston ring and wall and then wear of cylinder liner. Beside the minor causes by piston ring surfaces finishing and coating, cylinder liner material, cylinder liner surface finishing and coating and cylinder liner out of roundness.

The aim of the present work is to minimize side thrust force as it is major cause of cylinder liner wear.

In the present work an arrangement of twin crankshaft model has been manufactured in Sudan University of Science and Technology-College of Engineering as a solution attempt to overcome cylinder friction and then reducing cylinder wear.

Twin crankshaft engine uses two contra-rotating crankshafts, geared together, and connected to a piston through two connecting rods driven by one crankshaft.

Experimental work was carried out to investigate wear characteristics using three different engines arrangement inline, offset and twin crankshaft engines, for two engine's speeds.

A computer program was used to model the three engines arrangements and to obtain their theoretical performances.

A comparison between the experimental results of the three engines arrangement showed that twin crankshaft engine arrangement is a promising solution for reduction of cylinder liner wear. This is in agreement with the predicted results obtained by the computer program.

الخلاصة

محركات الاحتراق الداخلي التقليديةِ لاتزال تستخدم لأكثر من قرن. بسبب كفاء تها الهالية وكلفتها الهنخفضة.

الكفاءة الكلية لهذه الهحركات حوالي 50 %. هذا يَعْني بأنّ حوالي 50 % فقط من طاقة الوقود يتحول إلى عمل مفيد، والباقي عبارة عن طاقة مهدرة بسبب الاحتكاك بين الأجزاء المتحركة.

الاحتكاك أسوأ عدو للماكينات إذ أنه يُضعف المعادن ويهدر القدرة ويولد الحرارة. يَحْدثُ الاحتكاك في كُلّ الأجزاء الم تحركة في المحرك، مثل حلقات المكبس والمحامل والصمامات والحدبات، لكن الاحتكاك بين حلقات المكبس و مبطّن الأسطوانات مسئول عن حوالي نِصنف الطاقة الضائعة في الاحتكاك.

التلامس المنزلق بين حلق ات الهكبس و مبطّن الأسطوانة يُؤدّيانِ إلى حدوث آلياتِ احتكاك مختلفةِ أثناء دورةِ عملِ واحدة مِنْ المحرّك. و بسبب الاختلافات في الحملِ، السرعة، القأثيرات السطحيّة ، ظروف التزييت بين حلقات المكبس ومبطن الأسطوانة تكون عابرة ، الأمر الذي يؤدي إلى تفاوت في حدوث التآكل والاحتكاك.

التآكل في مبطّنِ الأسطوانة يؤدي إلى تقليل كفاءة حلقات المكبس التي تعمل كمانعة للتسرب ، وهذا قَدْ يُؤدّي إلى استهلاك متزايد للزيت ، تسرب غازات غرفة الاحتراق وبالتالي تقليل ضغط الاحتراق ، واستهلاك متزايد للوقود.

عيبب ضغطِ الاحتراق قوة على المكبس، المكوّن الأفقي لهذه القوة هو قوة الدفع الجانبية التي تؤثر عمودياً على سطح المبطّن. هذه القوة مسئولة عن الاحتكاك بين حلقات المكبس و مبطن الأسطوانة ومن ثم تؤدي اللي تآكل مبطّن الأسطوانة. إلى جانب الأسباب البسيطة الأخرى مثل صقل وطلاء سطوح حلقات المكبس، مادّة مبطّن الأسطوانة، صقل و طلاء مبطّن الأسطوانة و الأسطوانة غير مكتملة الاستدارة.

إنّ هدف العملِ الحالي هو تخفيض قوة الهفع الجانبية التي هي سبب رئيسي لتآكل مبطّن الأسطوانة. في العملِ الحالي تم تصنيع نموذج لماكينة ثنائية عمود المرفق في جامعة السودان للعلوه والقكنولوجيا كلية الهندسة لعمداولة لحل مشكلة الاحتكاك بين المكبس و الأسطوانة وبالتالي تخفيض تآكل الأسطوانة. الماكينة ثنائية عمود المرفق هي عبارة عن نظام يستخدم عمودي مرفق يدوران في اتجاهين متعاكسين

تمت كتابة برنامج حاسوبي لنمذجة الترتيبات الثلاثة للمحركات وللحصول على الأداء النظري لها.

ويتصلان بالمكبس عن طريق ذراعي توصيل يتم تدويرهما بواسطة عمودي المرفق.

العمل التجريبي نُفذَ لثلاثة ترتيبات لهحركاتِ مختلفة: الماكينة التقليدية والماكينة ذات عمود المرفق اللا متمركز وأخيرا الماكينة ثنائية عمود المرفق. عند سرعتين مختلفتين للهحرك.

أجريت مقارنة بين النتائج المتحصلة للمحركات الثلاث ووجد أن الماكينة ثنائية عمود المرفق تعد حلاً واعدا لتخفيض تآكل مبطن الأسطوانة. هذه النتائج جاءت متوافقة مع نتائج الهرنامج الحاسوبي.

Acknowledgment

I would like to thank many people whose help and encouragement and valuable advices, which made it possible to do this work.

Among those to whom I am especially indebted is

Professor

Uzaldin S. Abdulhussain

Who offered his time in supervision, follow up and guidance throughout the research period and during the preparation of this thesis.

Associate professor

Taj Elssir Hassan

For his unlimited help, constant indispensable and invaluable comments.

My thanks also to the staff of mechanical engineering and the staff of the workshop in the College of engineering of Sudan University of Science and Technology.

List of symbols:

g

h

Horsepower

Piston acceleration, m/s² a Rod's small end loading area, m² $\mathbf{A}_{\mathbf{bc}}$ Shank cross-section area,m² A_{N-N} Cylinder cross-section area, m² $\mathbf{A}_{\mathbf{p}}$ Connecting rod length, m b Cylinder diameter, m c Static load, N/m² \mathbf{C} Belt center distance, m C_h $\mathbf{C}_{\mathbf{F}}$ Surface condition factor $\mathbf{C_n}$ The elastic coefficient, √psi Specific heat, (kJ/kg.k) $\mathbf{C}_{\mathbf{v}}$ D Cylinder diameter, m Crankshaft offset from the axis of piston movement, m d Outer diameter of the main pin, m $\mathbf{D}_{\mathbf{bp}}$ Di Inner diameter of the main pin, m Inner diameter of big end pin, m $\mathbf{D_{in}}$ Rod's big end inner diameter, m $\mathbf{D_{is}}$ Rod's big end outer diameter, m \mathbf{d}_{op} Rod's small end outer diameter, m \mathbf{d}_{os} $\mathbf{d_{p}}$ Pitch diameter, m \mathbf{D}_{PL} Outer diameter of the big end pin, m $\mathbf{F}_{\mathbf{n}}$ Net face width, m F Force applying on the end of the crank arm, N Side thrust force, N $\mathbf{F}_{(\text{thrust})}$ Friction force, N $\mathbf{F_f}$ Gas force, N/m² $\mathbf{F}_{\mathbf{g}}$ Inertia force, N $\mathbf{f_i}$ fmep Friction mean effective pressure or work to over come friction, atm $\mathbf{F_r}$ Rod applied force, N Piston force, N $\mathbf{F}_{\mathbf{s}}$ Safety factor $\mathbf{f}_{\mathbf{s}}$ Gravity, m/s²

Н Life time for the bearing, hours $\mathbf{K}_{\mathbf{R}}$ Rim-thickness factor $\mathbf{K}_{\mathbf{m}}$ Load distribution factor $\mathbf{K}_{\mathbf{0}}$ Overload factor $\mathbf{K}_{\mathbf{s}}$ Shape factor $\mathbf{K}_{\mathbf{v}}$ Dynamic factor L The length between the centers of the big and small pins, m Rod's big end length, m L_{p} The length of the big end pin, m L_{PL} Rod's small end length, m $\mathbf{L}_{\mathbf{s}}$ Mass of the piston and piston's pin, kg m Work required to motor an engine, atm mmep Constant n N Force applying on the piston, N Gas pressure, N/m² P Power produced by the electric motor, W $\mathbf{P_h}$ Dynamic load applying on bearings, N P_{b} Diametric pitch, (1/in) P_d Heat addition, kJ Q Radius of crankshaft, m r R Gas constant, (kJ/kg.k) Radius of the big pulley, m $\mathbf{R}_{\mathbf{p}}$ Radius of the small pulley, m $\mathbf{r}_{\mathbf{p}}$ Temperature, C^o \mathbf{T} Rod's small end thickness, m t_{s} Velocity, m/s V

Greek symbols:

Volume, m³

Fraction of heat release

 \mathbf{V}

- lpha Angle between the extension of connecting rod and the line perpendicular to the crank arm, degrees
- γ Specific heat ratio
- Angle between the crank and the line joining the center of the crankshaft to the piston, degrees

μ Friction factor

 σ_b Load stress, N/m²

 σ_c Contact stress for the gear, N/m²

 σ_{cc} Compression stress, N/m²

 τ_{max} Maximum shear stress, N/m²

 ϕ The angle between the connecting rod and the axis of piston movement, deg

ω Angular velocity, rad/s

Subscripts:

b bearing

b belt

c contact

d diameter

g gas

i inner

ip Inner, big

max maximum

n net

o overload

op Outer, big

p pulley

r rod

s small

Table of content:

Abstı	ract		II		
Arab	ic abstra	ct	IV		
Ackn	owledgm	nent	VI		
List o	of symbol	s	VI		
Chap	oter one		1		
Intro	duction		1		
1.1	Prelimi	inary remarks	2		
1.2	Statem	ent of problem	3		
1.3	Scope and subject of present work				
1.4	Objecti	Objectives of present work			
Chap	oter two		9		
Line	rs wear, (Causes, effects and cures	9		
2.1	Introdu	action	10		
2.2	Factors	s affecting wear in engine's cylinder liners	12		
	2.2.1	Friction	12		
	2.2.2	Engine speed	14		
	2.2.3	Piston ring surface finishing and coating	15		
	2.2.4	Liner material	16		
	2.2.5	Cylinder liner surface finishing and coating	16		
	2.2.6	Side thrust force	17		
2.3	Compu	tational simulation	19		
2.4	Effect	of wear in engine's cylinder liners on engines performance	21		
	2.4.1	Combustion gases (blow-by)	21		

	2.4.2	Oil cons	sumption	22	
	2.4.3	Noise ar	nd vibrations	22	
2.5	Remed	dies of wear			
	2.5.1	Lubrication		23	
	2.5.2	Piston s ₁	Piston specifications		
	2.5.3	Piston ri	Piston rings		
	2.5.4	Rotating	g liner engine	28	
	2.5.5	Offset w	Offset wristpin		
	2.5.6	2.5.6 Offset crankshaft			
	2.5.7 Revetec engine			30	
	2.5.8	Twin cra	ankshaft engine	30	
		2.5.8. 1	Connecting rods affixed to one wrist pin	33	
		2.5.82	Connecting rod affixed to two spaced wrist pins	33	
		2.5.8. 3	Arced connecting rods	33	
		2.5.8. 4	Connecting rods in crossed configuration	34	
Chapter three 37					
Theo	retical ap	proach		37	
3.1	Introdu	ction		38	
3.2	Computer program			39	
	3.2.1 Program flow chart		n flow chart	40	
	3.2.2	Piston d	lisplacement, speed and acceleration	42	
		3.2.2.1	Inline crankshaft engine	42	
		3.2.2.2	Offset crankshaft engine	43	
		3.2.2.3	Twin crankshaft engine	45	
	3.2.3 Engines performance			45	
		3.2.3.1	Inline crankshaft engine performance	46	

		3.2.3.2	Offset crankshaft engine performance	51
		3.2.3.3	Twin crankshaft engine performance	53
	3.2.4	Theoret	ical torque	54
		3.2.4.1	Inline crankshaft engine performance	57
		3.2.4.2	Offset crankshaft engine performance	59
		3.2.4.3	Twin crankshaft engine performance	60
Cha	apter four			63
Exp	perimental 1	test rig		63
4.1	Introduction	Introduction		
4.2	Design of	of test rig		
	4.2.1	Connec	ting rod	65
		4.2.1.1	Small end and big end	66
		4.2.1.2	Shank	67
	4.2.2	Crank S	Shaft	68
		4.2.2.1	Crank big end pin	69
		4.2.2.2	Crank bearing pin	69
	4.2.3	Crankshaft flange		69
	4.2.4	Gears		70
	4.2.5	Liner		71
	4.2.6	Piston		71
	4.2.7	Pulley		71
	4.2.8	Bearing	selection	72
	4.2.9	Motor s	election	72
	4.2.10	Belt sel	ection	72

4.3	Measuring instruments			75
	4.3.1	Dial bor	re gauge	75
	4.3.2	Fernier		76
	4.3.3	Digital 1	palance	76
4.4	Test pro	ocedures		76
Chap	oter five			80
Results and discussions			80	
5.1	Introdu	ction		81
5.2	Compu	mputer programs results		81
	5.2.1	Effect	of engine with offset distance (d)	81
		5.2.1.1	(intake-power) strokes	81
		5.2.1.2	Piston displacement	84
		5.2.1.3	Piston speed	85
		5.2.1.4	Piston acceleration	85
		5.2.1.5	Angle phi	86
	5.2.2 Effect of (d), (r) and (b)			
		5.2.2.1	(Intake – exhaust) stroke	86
		5.2.2.2	Piston displacement	87
		5.2.2.3	Piston speed	88
		5.2.2.4	Piston acceleration	89
		5.2.2.5	Angle (phi)	90
	5.2.3	Motor	driven engines	91
		5.2.3.1	Inline crankshaft engine	91
		5.2.3.2	Offset crankshaft engine	92

	5.2.3.3 Twin crankshaft	92
	5.2.3.4 Comparison between the three arrangements	93
	5.2.3.4.1 Acceleration	93
	5.2.3.4.2 Side thrust force	94
	5.2.3.4.3 Force applied on piston	95
	5.2.4 Combustion driven engine	95
	5.2.4.1 Inline engine	95
	5.2.4.2 Offset engine	96
	5.2.4.3 Twin crankshaft	97
	5.2.4.4 Comparison between the three arrangements	97
	5.2.4.4.1 Torque	97
	5.2.4.4.2 Side thrust force	98
5.3	Experimental Results	99
	5.3.1 Wear characteristics	99
	5.3.1.1 Inline engine	99
	5.3.1.2 Offset crankshaft engine	110
	5.3.1.3 Twin crankshaft engine	120
	5.3.2 Comparison between the three arrangement	130
Chapte	er six	136
Conclu	sions and suggestions for future work	136
6.1	Conclusions	137
6.2	Suggestions for future work	138
Refere	nces	139

Appendices A	FORTRAN program used for calculating piston	143
	displacement, speed, acceleration and the angle $\boldsymbol{\phi},$ with	
	an offset crankshaft engine	
Appendices B	FORTRAN program used to get the inline engine	143
	performance	
Appendices C	FORTRAN program to calculate the offset crankshaft	144
	engine performance	
Appendices D	FORTRAN program to calculate the twin crankshaft	146
	engine performance	
Appendices E	Numerical solution of ordinary differential equations	147
Appendices F	Papers published during the course of present work	150