## Appendix A

## The load flow Algorithm in NEPLAN program:

The load flow problem is non-linear, because at every network node $i$, an apparent power $S_{i}$ is given:

```
Si=\mp@subsup{P}{i}{}+j\mp@subsup{Q}{i}{}=\mp@subsup{V}{i}{***}\mp@subsup{|}{i}{\prime}(*=\mathrm{ conjugate complex)}
```

The power Application software (PAS) is driven by off line and on line data, for study purposes, all functions of PAS can also be operated off line. Given:
a) off line data:

- Elements with impedances (lines/cables, transformer, generators) with limits of operation, these 2 terminal element are represented by their branch four-poles and the individual branch admittance matrices.
- Elements without impedances (bus-bar, circuit breakers isolators, CTs, PTs, etc) with limit of operation.
- Static network: topology (Node-Branch representation, static connection of elements without and with impedances, regardless of the positions of the circuit breaker and isolators).
- Generator and load data: attached to bus-bar node type: PQ, PV, Slack.
b) On Line: data:
- Actual network: topology (position of the circuit breakers and isolators, closed, open running, under-fined etc).
- Actual measuring values: at bus-bars for load flow additionally branch values for state estimation to be calculated:
a) All node voltages, voltage. Vector, vector of state variables define the actual steady state of the system.
b) Results derived from the state vector:
- Branch currents and powers, overload indication.
- Node voltages with indication of limit violation.
- Balances of active and reactive power, active and reactive losses.


## Application of the load flow Algorithm:

a) Off line for study purposes:

Function in NEPLAN 2000
b) On-line in PAS (power application software):

- SSE state estimation.
- Optimal load flow.
- CAN contingency analysis etc.


## Solution methods:

Overview: Gauss Seidel, current iteration, Newton-Raphson

## Causs- Seided:

Historical, no inversion of Y matrix needed:
a) Set state vector V to +j 0 pu (flat start).
b) For each node i DO:

V i is Calculated, the other Vj remain constant joint solution of:

$$
\begin{aligned}
& I_{i}=Y_{i i} * V_{i}+\sum \hat{Y}_{i j} * V_{i} \\
& \text { and } \\
& I i=\left(S_{i} / V_{i}\right)
\end{aligned}
$$

Special treatment of PV nodes. Slak node:
Vi is not changed
c) The calculation is stopped, if the hange of state vector is below a specified accuracy limit:

Much iteration is required, convergence of the iteration process is questionable, but storage requirement are small.

## Current Iteration method:

Basic: Factorized, Y - matrix
a) Set state vector $\underline{\mathrm{V}}$ to $\underline{1}+\mathrm{J} 0 \mathrm{pu}$ (flat start).
b) Repeat until convergence is reached.
b1) for each node i Do:

$$
\mathrm{Ii}=(\underline{\mathrm{S}} \mathrm{i} / \underline{\mathrm{V}})
$$

Special treatment of PV node. Slack in node: Vi is not changed.
b2) Network solution:
Solution of $\mathrm{V}=\mathrm{Z} * \mathrm{I}$ forward substitution
Result: New state vector Vnew
b3) Convergence check: the check: The calculation is stopped, if the change of the state vector is below a specified a currency limit.

b4) if convergence not yet reached it

$$
\text { Vi }=\text { Vnew }
$$

b5) END REPEAT.
Just a few iterations are required typically $4 \ldots 7$, even for large networks, convergence is in general reached, if there exists also a physical solution the problem and the static stability limit are not violated.

## Newton Raphson:

Priociple: minimization of a mismatch function:
Search for the point, defined by the state vector V, where the mismatch function zero.

The mismatch function in our case is the difference between the actual and the given nodal apparent powers:

$$
\begin{aligned}
& \Delta s_{i}=S_{,} \text {actual }-S_{i} \text { given } \\
& S_{i} \text { actual }=V_{i}^{\prime \prime *} * I_{i}^{\prime \prime}
\end{aligned}
$$

Because the Ii depend also from Vi, the first term in the above equation is nonlinear in Vi. All deviations as are caused by deviations in the state variables, $\Delta_{v}$ and we can make a formal linearization a round the working point:

This can be illustrated by fig below:


Because the (partial) derivative is not defined for complex numbers all values $\underline{S}=P+j Q, \underline{\mathrm{~V}}, \underline{\mathrm{I}}, \underline{\mathrm{Z}}, \underline{\mathrm{Y}}$ must be broken down intro real numbers either is Cartesian or in polar coordinates.

In this case the matrix describing the partial derivatives in *(A) is a real matrix with the dimension $2 \mathrm{~N}^{*} 2 \mathrm{~N}$ and is called it or Jacobian (Jacobi's matrix).

The vectors of power and voltage differences have the dimension 2 N each.

According to *(A) the change of the state vector $\Delta v \quad$ can be calculated by multiplying the inverse of $\mathrm{H}, \mathrm{H}^{-1}$ with the given power mismatches Si .

## Discretion of iteration:

a) Set state vector V to $1+\mathrm{j} 0$ pu (flat start).
b) Repeat until convergence is reached.
b1) for each node i Do:

$$
\begin{gathered}
\mathrm{I}_{\mathrm{i}} \text { by using } \\
\mathrm{S}_{\text {iactual }}=\mathrm{Vi}^{*} * \mathrm{I}_{\mathrm{i}} \text { and } \mathrm{S}_{\mathrm{i}} \text { actual }=\mathrm{S}_{\mathrm{igiven}} \\
\Delta_{s i} \text { by using } \\
\Delta s_{i}=\mathrm{S}_{\text {iactual }}=\mathrm{S}_{\text {igiven }}
\end{gathered}
$$

Special treatment of PV nodes slack node:

## $V_{i}$ is not changed

b2) Network solution:
Setup of H and factorization:
for each iteration step or:
set up of H and factorization once at the beginning (constant slope).
Solution of *(A) by for word and backward substitution result new state vecor Vnew $=$ Vold $+\Delta V$
b3) convergence check: The calculation is stopped if the change of the state vector is below a specified accuracy limit.
b4) if convergence not yet reached:

$$
\text { Set } \underline{\mathrm{V}}_{\mathrm{i}}=\underline{\mathrm{V}}_{\text {new }}
$$

## b) END REPEAT:

Just a few iterations are required (typically 4.....7, even for large network).

Convergence is in general reached, if there exists also a physical solution to the problem and the static stability limits are not violated.

In order to minimize the calculation burden several treatment of H are in use:

- Decoupled load flow: only the dependence of P on the voltage angles and of Q on the voltage magnitudes is considered.
- H calculated factorized once, only after a certain number of iterations or at each iteration.
- etc. etc.


## APPENDICES B

## NEPLAN DATA

## LOAD DATA:

| Name | P/MW | Q/MVAR |
| :--- | :---: | :---: |
| Atbara (NEC) 220kv | 68 | 42.140 |
| Aroma | 4.25 | 2.630 |
| Banat 110 | 46.750 | 28.970 |
| Eldebba 220 | 12.750 | 7.900 |
| Dongle 220 | 32.2 | 21.070 |
| Eid Babker 110 | 42.500 | 26.340 |
| Elbager 110 | 4.250 | 13.750 |
| Elfao 110 | 11.333 | 2.630 |
| Elgriba 220 | 21.250 | 2.578 |
| Elobeid 220 | 42.500 | 20.170 |
| Faroug 110 | 59.500 | 36.870 |
| Free zone | 17.659 | 8.713 |
| Elgederef 110 | 51.500 | 30.000 |
| Gamuoia | 10.590 | 20.00 |
| Giad 110 | 42.500 | 5.270 |
| Hag Abdallah 110 | 12.500 | 5.340 |
| Hassa Heisa | 85.000 | 52.680 |
| Hawata 220 | 58.244 | 21.038 |
| Izergab 110 | 127.500 | 68.570 |
| Jebel Aulia 110 | 12.108 | 5.270 |
| Khartoum East 110 | 127.501 | 79.02 |
| Kassala 220 | 6.293 | 5.669 |
| Khartoum North 110 | 42.500 | 19.340 |
| Kilo3 66 | 59.500 | 36.870 |
| Kilox 110 | 101.000 | 53.750 |
| Kuku 110 | 58.500 | 38.460 |
| Local market 110 | 43.000 | 26.340 |
| Mahadia 220 | 21.250 | 17.662 |
| Mahadia 110 | 12.750 | 7.900 |
| Managil | 51.000 | 35.610 |
| Mashkur | 6.500 | 5.270 |
| Maringan 110 | 19.496 | 10.540 |
| Merowe town | 14.450 | 6.960 |
| Mina sharif 110 | 103.000 | 60.020 |
| New Halfa | 76.500 | 47.410 |
| Mugran 110 |  |  |
| Omdurman 110 |  |  |


| Name | P/MW | Q/MVAR |
| :--- | :---: | :---: |
| Port Sudan | 10.000 | 11.070 |
| Rabak 110 | 17.250 | 10.540 |
| Rank 220 | 4.250 | 2.630 |
| Rawashda | 5.530 | 3.930 |
| Sennar 110 | 25.504 | 10.578 |
| Shagara 110 | 71.911 | 52.680 |
| Shendi 220 | 18.000 | 13.700 |
| Singa 220kv | 9.874 | 6.862 |
| Tandulti 220 | 12.750 | 7.850 |
| Umrawaba 220 | 8.500 | 5.270 |

